References

[1] Mei, C., "A Finite-Element Approach for Nonlinear Panel Flutter," *AIAA Journal*, Vol. 15, Aug. 1977, pp. 1107-1110.

[2] Mei, C., "Nonlinear Vibration of Beams by Matrix Displacement Method," *AIAA Journal*, Vol. 10, March 1972, pp. 355-357.

[3] Mei, C., "Finite Element Displacement Method for Large Amplitude Free Flexural Vibrations of Beams and Plates," *International Journal of Computers and Structures*, Vol. 3, Jan. 1973, pp. 163-174.

Reply by Author to G. Prathap

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THE author would like to thank Prathap for his interest in the work and for his relevant remarks. He is correct in the assumption of immovable edge conditions, which are employed widely in nonlineear fluttering panels. However, the author would like to add that the axial loading N_{xo} could also be due to change in temperature. The author is also thankful to Prathap for bringing out a few clarifications in the assumptions on membrane force N_x. The author is now modifying the computer program, and new results will be presented later.

Errata

Modeling of Convective Mode Combustion through Granulated Propellant to Predict Detonation Transition

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THE total energy per unit mass e for both the gas phase and solid phase should include the kinetic energy as well. Thus, in Eq. (10),

$$e_g = c_{v_g} T_g + u_g^2/2$$

and in Eq. (11),

$$e_p = c_{v_p} T_p + u_p^2/2$$

This also means that the last term in each of the field balance energy equations (10) and (11), describing the gas-particle heat transfer, should read, respectively

$$\mp \bar{h}[3\alpha_2(T_g - T_p)]/r_p$$